

**Melt Spun Thermoplastic Polyurethanes Useful as Textile Fibers**

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## **Field of the Invention**

The present invention relates generally to the preparation of melt spinnable thermoplastic polyurethane elastomers and, more specifically, to the preparation of polyurethane elastomers utilizing a novel multi-step polymerization process.

## **Background of the Invention**

Melt-spun elastomeric fibers have been in the past unacceptable for use as textile fibers because they have very low tenacity and poor recovery from elongation. Also melt-spinnable thermoplastic urethane polymers have in the past formed gels too readily, thus inhibiting spinning of the material.

Prior art methods of forming melt-spun polyurethane fibers include the use of a "one shot process" wherein mixtures of diisocyanates, a polymeric glycol "soft" segment, and a low molecular weight glycol and a catalyst are all added to an extruder with mixing at a temperature of about 100°C to about 250°C and a time of about 1-5 minutes to obtain, after spinning, a polyurethane fiber. The properties of this fiber are limited because of the randomness of the polymerization process, the required rapid reaction and the substantially poor mixing. The urethane groups in the final product have no orderly arrangement, causing poor tenacity, unacceptable recovery from elongation and an unacceptable

amount of gel formation.

The preparation of plastics in extruders is generally known. In contrast to the processing of plastics by a purely thermoplastic method, the term “reaction extrusion” is used in the case of such polymer synthesis in an extruder. Accordingly, the extruder used as the chemical reactor is frequently also referred to as a “reaction extruder”.

Almost without exception, the literature recommends the twin-screw extruder in which both screws rotate in the same direction, for the synthesis of polyurethanes. Single-screw extruders and twin-screw extruders having counter-rotating screws are unsatisfactory owing to the poor mixing effect during passage through the extruder, and extruders having more than two screws are too expensive.

U.S. Patent No. 5,621,024 (Eberhardt, et al) discloses a process for preparing thermoplastic polyurethane employing a twin-screw extruder having multiple zones. All reactants are fed as a low viscosity mixture to the extruder in a “one shot” process.

U.S. Patent No. 5,136,010 (Reisch, et al) discloses a method of preparing a cast polyurethane or polyurea elastomer. The method comprises the steps of : fabricating a polyol having a specified molecular weight, reacting the polyol with a polyisocyanate to obtain an isocyanate-terminated prepolymer, and reacting the prepolymer with a non- (ethylene glycol) chain extender. The elastomer is prepared in a “one shot” process.

U.S. Patent No. 5,116,931 (Reisch, et al) discloses a thermoset polyurethane or polyurea elastomer prepared in a “one shot” process.

5 U.S. Patent No. 5,096,993 (Smith, et al) discloses a thermoplastic polyurethane or polyurea elastomer made by reacting in a “one shot” process a polyether diol, diisocyanate, and a chain extender. The Chain extender is a difunctional, isocyanate-reactive material.

10 U.S. Patent No. 3,233,025 (Frye, et al) discloses a method of forming a thermoplastic polyurethane having free isocyanate groups. The method comprises the steps of mixing reactive components comprising an excess of an organic polyisocyanate and an organic compound containing at least  
15 two active hydrogen containing groups, reacting in a passageway at a temperature of about 60°C to about 250°C and a limited residence time, and removing the thermoplastic polyurethane. A twin-screw extruder can be employed.

### 20 **Summary of the Invention**

In one aspect, the present invention relates to a melt spinnable thermoplastic polyurethane elastomeric polymer made by a three-step process. Fibers prepared from the polyurethane elastomer have a tenacity above about 0.6gm/denier, an  
25 elongation above about 400%, a percentage set from 200% stretch below about 10%, and gels of below about 1 ppm in the melt. An advantage of the melt spinning is the ability to make a

large range of sizes, all of which can be round, which is in contrast to the dry spinning processes.

The polyurethane fiber of the present disclosure exhibits unique structural properties on the molecular level. These properties allow the fiber to imitate the physical properties of well-known poly(ester)urea urethanes or poly(ether)urea urethanes such as Lycra®Spandex. The molecular structure of the fibers of the present disclosure reveals relatively similar lengths of “soft” segments spaced at substantially equal distance (by relatively similar lengths of “hard” segments) along the polymeric chain. The resulting configuration is an orderly arrangement of blocks of “hard” segments and blocks of “soft” segments. The orderly arrangement, unachievable in a conventional “one shot” process, gives the polyurethane fiber the qualities of high tenacity, high elongation and low set.

The molecular polarity of the polyurethane fiber of the present disclosure is weaker than the polarity of the Lycra®Spandex molecules because of a substantial lack of urea functionality in the polyurethane molecules. In order to compensate for this diversity in polarity, the present polyurethane fiber has a substantially higher molecular weight than Lycra®Spandex molecules.

A process for preparing a melt spinnable elastomeric polyurethane polymer is disclosed. The process comprises the steps of : preparing a first poly(ether)urethane oligomer (or poly(ester)urethane oligomer); preparing a second poly(C<sub>2</sub>-C<sub>6</sub>

glycol)urethane oligomer; and reacting in a reaction extruder, under relatively high mixing conditions, the first “soft” oligomer and the second “hard” oligomer. The final product is a poly(ether)urethane polymer or a poly(ester)urethane polymer containing an orderly arrangement of blocks of “hard” segments and blocks of “soft” segments. The term “polyurethane polymer” includes poly(ether)urethane polymer, poly(ester)urethane polymer, and poly(ether-ester)urethane polymer. These and other aspects of the invention will become apparent upon reading the following detailed description of the invention.

### **Detailed Description of the Invention**

The present disclosure relates to a melt spinnable composition useful in preparing textile fibers. The composition comprises a high molecular weight polyurethane polymer prepared from conventional starting materials. The polymer is prepared from at least two diol monomers wherein the two diol monomers are always reacted separately, and never in a “one shot” process.

The two diol monomers, which are always to be reacted separately, are: a first diol monomer of relatively high molecular weight and a second diol monomer of low molecular weight. The second diol monomer preferably has terminal hydroxyl groups, and has a molecular weight of about 62 to 122. The first diol monomer preferably has terminal hydroxyl groups, and has a molecular weight of about 1,000 to about

8,000. In a preferred embodiment, the first diol monomer is a member selected from the group consisting of a polyether diol, a polyester diol and a mixed polyether-polyester diol.

The separate reaction of the two diol monomers are conducted in both cases with a diisocyanate monomer reactant. In a preferred embodiment, the diisocyanate monomer reactant is the same in both cases. Included within this preferred embodiment is the process wherein the same mixture of two or more diisocyanate monomers is employed.

The diisocyanate monomer preferably has terminal isocyanate groups, and the diisocyanate can be aliphatic or aromatic. Isomeric mixtures of diisocyanates can also be employed. Examples of diisocyanate monomers are 1, 6-hexane diisocyanate, all isomers of toluene diisocyanate, and methylene diisocyanate.

The reaction between the second low molecular weight diol and the diisocyanate yields a product that is solid and potentially hard to melt. The length of the polymer chain which is prepared from the low molecular weight diol must be carefully controlled. Otherwise, the "hard segment", prepared from the low molecular weight diol and a diisocyanate, becomes intractable during the melt spinning process.

After the separate reactions of the two diol monomers are conducted, the two products are worked up and purified, if desired. When these two products are combined under reaction conditions in a reaction extruder along with suitable catalyst, a final polyurethane polymer product is obtained. The

polyurethane polymer has a molecular weight of about 100,000 and above, and preferably about 200,000 and above. The tenacity of the polymer is about 0.6 grams/denier and above. The elongation of the polyurethane polymer is about 400% and above. All of the above properties are present in fibers prepared from said polyurethane polymer.

The high molecular weight polyurethane polymers contain "hard" segments and "soft" segments arranged in an orderly, non-random fashion. The "hard" segments are a product of the reaction between the second low molecular weight diol monomer and a diisocyanate. The "soft" segments are a product of the reaction between the first high molecular weight diol monomer and a diisocyanate monomer.

The melt spinnable composition containing the high molecular weight polyurethane polymer can be prepared by a process comprising the steps of: obtaining a polyol prepolymer which is a member selected from the group consisting of polyether diols, hydroxyl terminated polyester glycols, hydroxyl terminated polyether/polyester glycols, and mixtures thereof; adding to the polyol prepolymer a first organic diisocyanate to obtain a first mixture. The first mixture is then reacted under suitable reaction conditions to obtain a first polymer. This first polymer will become the "soft" segment in the final high molecular weight polyurethane polymer.

The process is then continued by obtaining a low molecular weight glycol; adding the glycol to a second organic diisocyanate to obtain a second mixture. The second mixture is



then reacted under suitable reaction conditions to obtain a second polymer. The second polymer will become the “hard” segment in the final high molecular weight polyurethane polymer.

5 This second polymer typically has a molecular weight low enough to be metered to the reactor extruder. Viscosity must be controlled to allow the second polymer to be combined with the first polymer in a reaction extruder. This can be accomplished by reacting the low molecular weight diol with a  
10 suitable diisocyanate under conditions to maintain production of a second polymer of sufficiently low molecular weight.

To continue the process, the first polymer is combined with the second polymer in a reaction extruder under suitable reaction conditions. In a preferred embodiment, the mole ratio of isocyanate functionality to hydroxyl functionality in the  
15 combination of polymers is about 0.98:1 to about 1.2:1. A final product of high molecular weight polyurethane is withdrawn from the reaction extruder.

20 The process further comprises the steps of pelletizing the solid high molecular weight polyurethane, melting the pelletized material and then spinning the melted polyurethane into elastomer fibers.

25 In an alternative embodiment, the solid product withdrawn from the reaction extruder can be pelletized, melted, and then spun as a fiber into a vaporous low molecular weight aliphatic diamine. The fiber, as a result of this treatment, will have a minor amount of urea functionality.

In yet another alternative embodiment, the solid product withdrawn from the reaction extruder can be pelletized, melted, and then spun as a fiber into an aqueous solution of low molecular weight aliphatic diamine. Once again, the fiber will then have a minor amount of urea functionality.

In reference to the process step of adding a first organic diisocyanate to the polyol prepolymer, the mole ratio of isocyanate groups to hydroxyl groups in the mixture is preferably about 1.2 to about 1:1.1. The mixture is then preferably heated at a temperature of about 60°C to about 100°C and at atmospheric pressure for a time of about 20 minutes to about 100 minutes.

In reference to the process step of adding a second organic diisocyanate to the low molecular weight glycol, the mole ratio of isocyanate groups to hydroxyl groups in the mixture is preferable about 1:2 to about 1:1.2. The mixture is then preferably heated at a temperature of about 50°C to about 70°C and at atmospheric pressure for a time of about 2 minutes to about 10 minutes.

In reference to the process step of combining the first “soft” polymer with the second “hard” polymer in a reaction extruder, the two polymers are contacted in the reaction extruder along with excess diisocyanate to obtain a ratio of free isocyanate groups to free hydroxyl groups of about 1:1 under high mixing conditions and a temperature of about 125°C to about 260°C for a time of about 2 minutes to about 8 minutes and at atmospheric pressure. The three-step process depends on

the use of a controlled polymerization reaction to obtain a meltable form of the second polymer ("hard segment"), prepared from the low molecular weight diol and a second diisocyanate, for addition to the first polymer ("soft segment") in the reaction extruder. The final polyurethane polymer product can then be withdrawn from the reaction extruder, pelletized, melted, and spun into fibers.

The low molecular weight glycol preferably contains 2 to about 20 carbon atoms. Typical examples of such glycols include ethylene glycol, propylene glycol, 1, 6-hexane diol, 1, 4-butanediol, neopentyl glycol, diethylene glycol, thiodiglycol, 2, 2-dimethyl-1, 3-propylene glycol, and the like. In a most preferred example, the glycol is a C<sub>2</sub>-C<sub>6</sub> glycol.

The polyol prepolymer preferably has a molecular weight of about 1000 and above, most preferably about 2000 to 6000. Such a prepolymer can be a chain extended polyester made from a glycol, preferably a mixture of ethylene and butylene glycols, and a saturated organic dicarboxylic acid, preferably adipic acid. The acid usually contains 4 to 20 carbon atoms. Typical examples include succinic acid, maleic acid, dihydromalonic acid, thiodipropionic acid, adipic acid, methyl adipic acid, glutaric acid, dimerized linoleic acid, sebacic acid, suberic acid, phthalic acid, and terephthalic acid. To some extent hydroxycarboxylic acids or their lactones can be used, eg., caprolactone, to aid in forming the polyesters. As stated, mixtures of various dibasic acids and glycols can be used to form mixed esters.

An excess of the glycol over the acid is used in preparing the polyesters so that the resulting polyester contains terminal hydroxyl groups. In general, the most suitable polyesters are chiefly linear with melting point levels of 20°C or lower and preferably not over 30°C. Less suitably natural polyesters can be used, eg., castor oil, as well as blown drying oils such as blown tung oil, linseed oil and soya oil.

As an alternative to the polyesters there may be used for reaction with the diisocyanate one or more elastomer yielding polyethers. Such polyethers are typically anhydrous chain extended polyethers possessing ether linkage separated by hydrocarbon chains either alkyl or aryl in nature. The ether should also contain terminal groups reactive to isocyanate, such as alcoholic hydroxyl groups. Such polyethers should be linear with a second order transition point of not over 25°C, preferably not over 10°C. The molecular weight range is from 500 – 7000, but preferably is within the range of 1000 to 5000. Preferred polyethers have the formula  $H(OR)_nOH$  where R is a lower alkylene group (2 to 6 carbon atoms) and  $n$  is an integer so that the molecular weight falls within the range specified. Examples of polyethers are polyethylene glycol, polypropylene glycol, polybutylene glycol, mixed polyethylene glycolpolypropylene glycol, polytetramethylene glycol (eg., of 1000 molecular weight).

Polyethers not only can be used in place of the polyesters but can be used in conjunction therewith. Examples of such compounds are polydiethylene glycol adipate. Further

examples of polyesters and polyethers which are suitable are set forth in Kohn Patent 2,953,839 and the patents cited therein (column 2, lines 56-68).

Long lengths of "soft" segments are desired. In the fiber prepared from the final polyurethane elastomeric product, the "soft" segments regulate the elongation of the fiber and the recovery from stretch of the fiber. In order to obtain long lengths of "soft" segments, higher molecular weight diols can be employed. Another approach to achieving long lengths of "soft" segments is to regulate the capping ratio so that the mole ratio of isocyanate to hydroxyl is in the range of about 1:2 to about 1:1.1. This cannot be done in the "one-shot" process.

The "soft" segments are oligomeric or polymeric and comprise blocks of polymeric glycol (poly)urethanes end capped with isocyanate groups. The "hard" segments are oligomeric or polymeric and comprise blocks of low molecular weight C<sub>2</sub> - C<sub>6</sub> glycol (poly)urethanes having free hydroxyl end groups. Both the "soft" segments and the "hard" segments are structured so that they can chemically interact with one another under suitable polymerization conditions to obtain a final TPU (thermoplastic urethane) polymer.

Representative of the preferred aromatic diisocyanates which may be mentioned, by way of non-limiting examples are m- and p-phenylene diisocyanate, tolylene diisocyanate (65% 2, 4 and 35% 2, 6), p,p' - diphenylisocyanate, 1, 5 naphthalene diisocyanate, p, p' -diphenyl-methane diisocyanate, 3, 3' - bitolyene-4, 4' -diisocyanate, 2, 4-tolylene diisocyanate dimer,

dianisidine diisocyanate, 4-chloro-1, 3-phenylene diisocyanate. Aliphatic and cycloaliphatic diisocyanates can also be used, such as 1, 4-tetramethylene diisocyanate, 4, 4'-methylene-bis (cyclohexylisocyanate), and 1, 5-tetrahydronaphthalene diisocyanate. Other diisocyanates can be employed including those set forth in the Kohn Patent, as well as those mentioned in the patents set forth in Kohn. The preferred diisocyanate is tolylene diisocyanate.

The vaporous low molecular weight aliphatic diamine generally has the formula  $H_2N-A-NH_2$ , where A is a divalent organic radical in which the terminal atoms are carbon, and which is devoid of groups reactive with isocyanate. As suitable amines there can be used ethylene diamine, hexamethylene diamine, 1, 4-diaminocyclohexane, p-phenylenediamine, 3-3' diaminodipropyl ether, diaminodibutyl sulfide, propylene diamine. The preferred diamine is ethylene diamine.

Preferably, catalysts are employed in the final step of the three-step process to obtain a final polyurethane elastomeric product. Examples of catalysts are triethylamine, cobalt naphthenate, stannous chloride, tetra-n-butyl tin, stannic chloride, tri-n-butyl tin acetate, n-butyl tin trichloride, trimethyl tin hydroxide, dimethyl tin dichloride, and di-n-butyl tin dilaurate. Because of the short residence time of the reactants in the reaction extruder during the final step of the three-step process, and also because of the relatively small volume inside the extruder, catalysts are usually necessary in order to speed the reaction and obtain high molecular weight thermoplastic

polyurethanes. An extruder of relatively low volume is required to allow for good mixing conditions under standard power requirements.

Any conventional extruder can be employed in the process of preparing the final polyurethane elastomer product. The reaction extruder preferably employs a twin-screw, co-rotating, self-wiping, multi-heating zone design. In a preferred embodiment, the extruder has a length to diameter ratio of about 46:1 and greater. The free volume in the extruder should allow for a residence time of about 2 minutes to about 8 minutes. Extruders made by Bersdorff or Davis Standard are acceptable for use.

The ratio of the reactants, the temperature of the reaction, and the time of the reaction are all critical factors in determining the length of the first "soft" segment, which ultimately regulates the elongation and recovery properties of the fiber. The length of the first "soft" segment can be in multiples of the starting polyol; so that if the starting polyol has a molecular weight of about 2000, then the length of the "soft" segment, when prepared under proper conditions, can contain some segments from 10,000 to even about 40,000 molecular weight. The proper conditions include an isocyanate to hydroxyl ratio of about 1:2 to about 1:1.1. "Soft" segments having molecular weights which are multiples of the molecular weight of the starting polyol can be formed when the isocyanate to hydroxyl ratio is less than about 1:2. This is because some of

the molecules have one end with an isocyanate group and one end with a hydroxyl group, making them self-reactive.

In an alternative embodiment, a thermoplastic polyurethane elastomeric polymer having sufficient lengths of "soft" segments can be prepared from a two-step process. An adequate alignment of "soft" segments and "hard" segments is obtained in the final polymer. In a first step, a prepolymer is formed from a diisocyanate and polyether diol, a polyester diol, a mixed polyether-polyester diol or mixtures thereof. This prepolymer has "soft" segments of a diol end capped with diisocyanate groups. The first step is performed with good mixing and in a time of about 20 minutes.

In this alternative embodiment, only one prepolymer is prepared, and that prepolymer is the "soft" segment. The second step requires the addition of the prepolymer to a reaction extruder along with more diisocyanate and a low molecular weight glycol. Preferably, a catalyst is also added to the mixture in the reaction extruder. Catalysts can be selected from the group listed above in the disclosure of the three-step process. The reaction in the extruder includes both the "in situ" formation of "hard" segments and the formation of the final thermoplastic polyurethane elastomer having well-defined blocks of "soft" segments and random blocks of "hard" segments. The compounds added to the reaction extruder in the two-step process are adjusted in amount so that the mole ratio of isocyanate to hydroxyl approaches 1.000, with the proviso that gel formation should be avoided. The temperature of the



reaction extruder should be controlled within the range of about 200°C to about 250°C.

In a modification of the two-step process, all of the diisocyanate necessary for formation of both the “soft” segment and “hard” segment can be added at once, during the first step. The product mixture obtained after the first step contains a first polymer (“soft segment”) and unreacted diisocyanate. The product mixture from the first step is added to a reaction extruder in a second step along with a low molecular weight glycol. Optionally, a catalyst can also be added to the extruder. Under appropriate reaction conditions, the second polymer (“hard segment”) is formed “in situ” and then a final thermoplastic polyurethane (TPU) elastomer is formed.

Fibers prepared from the TPU (thermoplastic urethane) elastomeric compositions of the two-step process do not have physical properties identical to the fibers prepared from polymeric compositions prepared according to the three-step process. However, the physical properties of both the “two-step process” fibers and the “three-step process” fibers are adequate for the manufacture of textile materials and the like. The two-step process requires less equipment and less control than the three-step process.

In both the two-step process and the three-step process, the physical properties of the fibers are dependent on the following parameters: (1) the ratio of “hard” segments in the polymer backbone; (2) the uniformity of the distribution of blocks of “hard” segments and blocks of “soft” segments in the

polymeric backbone; (3) the length of the “soft” segment in the polymeric backbone; and (4) the post-treatment regimen (e.g., stretching, heat setting, and the like conducted on the fiber).

All the parameters disclosed above are to be considered when a manufacturer produces a TPU elastomeric polymer composition suitable for melt spinning into fibers useful in the textile industry. Any of the parameters can be varied within certain ranges in the interest of economics and still obtain useful fibers.

The multi-step processes disclosed above have many advantages over the prior art processes as presented in the literature. Both multi-step processes disclosed above yield a melt spinnable polymeric material. There is no need or limited need for the use of solvents, and therefore the processes are environmentally friendly. The polymers prepared according to the multi-step processes herein disclosed have a combination of high tenacity, high recovery from stretch, high elongation and freedom from any gels greater than 20 micrometers.

All prior art one-shot processes cannot produce the necessary alignment of “soft” segments and “hard” segments. A one-shot process is when all reagents (polyol, glycol, diisocyanate and catalyst) are metered simultaneously into a reaction extruder. The products are polyurethanes from polymeric glycols and low molecular weight glycols, said products having random distributions of urethane linkages in the polymeric backbone. There is no adequate alignment of “soft” segments and “hard” segments, as all reactions in the

extruder are completed in a random fashion and usually in less than three minutes. When such a situation exists, small amounts of materials reach a molar ratio of isocyanate to hydroxyl of exactly 1.000. When such a ratio is reached, a polymer of "infinite" molecular weight is formed (gels). It is practically impossible to prevent such a situation when a one-shot process is employed.

One-shot processes are usually conducted at a temperature of about 125°C to about 260°C and at a time of about 3 minutes. Only one reaction extruder is employed, and no prepolymers are formed (except for the uncapped polyol). The final TPU elastomeric product contains only random alignments of "hard" segments and "soft" segments. The one-shot processes lack the ability to precisely control the desired high molecular weights.

In the multi-step processes herein disclosed, choice of catalyst greatly affects the reaction rate of the isocyanate and hydroxyl group. For example, if an uncatalyzed reaction of isocyanate with hydroxyl group is designated as having a reaction rate of 1, then the reaction rates of isocyanate with hydroxyl group for various catalysts are as follows: triethylamine (11), cobalt naphthenate (23), stannous chloride (68), tetra-n-butyl tin (82), stannic chloride (99), tri-n-butyl tin acetate (500), n-butyltin trichloride (83), trimethyl tin hydroxide (1800), dimethyltin dichloride (2100), and di-n-butyl tin dilaurate (37000). Also, undesirable side reactions of the isocyanate with water are suppressed by the use of a catalyst.

With the use of dibutyltin diacetate, the rate of reaction of isocyanate with hydroxyl group as compared to the reaction of isocyanate with water is about 6:1.